ALASKA	
by	
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Field report ************************************	

MINERALIZATION IN THE COAL CREEK TIN PROSPECT, SOUTH-CENTRAL

UNITED STATES DEPARTMENT OF THE INTERIOR Manuel J. Lujan, Jr. Secretary

BUREAU OF MINES TS Ary, Director

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UNITS OF MEASURE AND ABBREVIATIONS USED IN THIS REPORT

An Anorthite o Degrees

DDH Diamond drill hole

C Centigrade cm Centimeter kb Kilobar m Meter

Ma Million years before present

Mi Mile

Wt.% Weight percent

MINERALIZATION IN THE COAL CREEK TIN PROSPECT, SOUTH-CENTRAL ALASKA

By Tracy V.L. Parker¹

ABSTRACT

The Coal Creek tin prospect is located in the central Alaska Range, south-central Alaska. In 1982 Billiton Exploration USA identified 5 million metric tons of 0.2 percent tin with significant silver credits. Mineralization is hosted by two texturally and chemically distinct granite units: (1) a seriate granite porphyry which is intruded at depth by (2) a fine-grained granite porphyry. The contact between the two units is marked by a 1-3 meter zone of crenulate and dendritic crystals. Greisen alteration is centered in the upper seriate granite and only extends 10-20 meters into the fine-grained granite.

The granite units are very evolved with differentiation indices ranging from 91-97. They are also peraluminous but are still considered "I-type" igneous source granites.

The most important tin mineral is cassiterite. Stannite, sphalerite, arsenopyrite, pyrrhotite, pyrite, marcasite, loellingite, bismuthinite, chalcopyrite, and galena are also present. This mineral assemblage suggest a low oxidation and sulfidation state during mineralization. The majority of the ore minerals are located in, or near vertical 0.5 to 2.0 cm veins and their associated greisen alteration envelopes.

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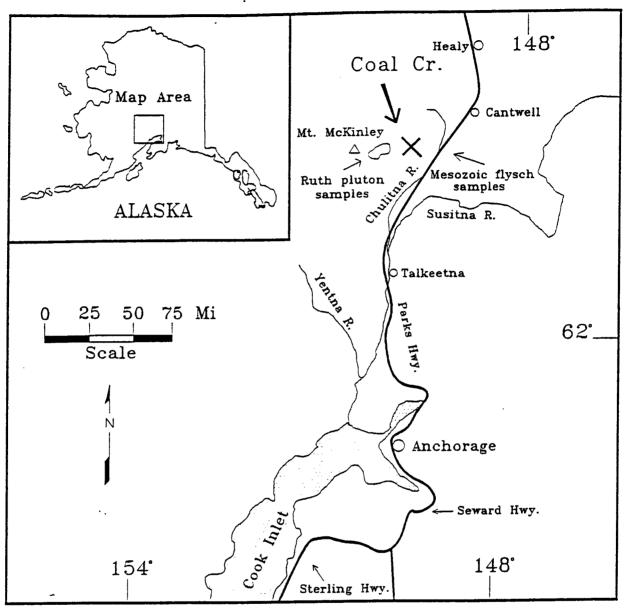


Figure 1. -Location map of the Coal Creek tin prospect.

INTRODUCTION

The Coal Creek tin prospect is located on the northwest side of the Chulitna River valley in the Talkeetna Mountains D-6 quadrangle (Sec. 21, T. 22 S., R. 12 W.) of southcentral Alaska (fig. 1). Coal Creek is within the Chulitna subdistrict of the Valdez Creek Mining District.

Study of the Coal Creek tin prospect has been supported by the U.S. Bureau of Mines as part of their ongoing project to evaluate Alaska's strategic and critical mineral resources. Tin is classified as a strategic mineral because the United States relies heavily on foreign sources of this commodity, and because it is used in defense-related

technologies.

There is no direct road access to the Coal Creek prospect. The Parks Highway and Alaskan Railroad lie on the east side of the Chulitna River five miles to the southeast of the prospect. The prospect is located on a small brush covered knob on the side of a steep, talus-covered mountainside. Rock exposure is poor and consists of approximately 4,000 square meters of mineralized greisen-altered granite. The granite intrudes Devonian metasediments of the Chulitna sequence, locally producing hornfels and skarn.

In the summer of 1982 Billiton Exploration USA drilled 42 holes totalling over 20,000 feet into the granite and sediments of the prospect (fig. 2). Although 42 holes were drilled many intersected barren hornfels and are not included in figure 2. Billiton Exploration USA later gave the core to the U.S. Bureau of Mines for study. Because Alaska is endowed with the bulk of the United States tin resources, investigating the characteristics and manifestations of the igneous-hydrothermal tin mineralizing processes provides parameters to guide future exploration initiatives. The drill core and data available from the Coal Creek deposit offered a unique opportunity to investigate the intimate relationship between multiple igneous units and mineralizing processes of an Alaskan tin deposit. Appendix A and B lists pertinent location and analytical data for drill core collected by Billiton Exploration USA.

ACKNOWLEDGMENTS

Thanks are extended to Billiton Exploration USA for allowing access to their drill core and data from Coal Creek. Technical reviews and discussions with Dr. Rainer Newberry, Associate Professor of Geology, University of Alaska Fairbanks, and Roger Burleigh, Geologist, U.S. Bureau of Mines Alaska Field Operations Center, Anchorage Branch helped considerably with the organization and interpretations presented in this report.

PREVIOUS WORK

The Coal Creek tourmaline granite was first reported to the U.S. Bureau of Mines by C.C. Hawley. In 1977 Bruce Reed (USGS geologist) visited the site and identified it as a greisen-altered desseminated tin occurrence. Two granitic rock types were identified and presumed to be genetically linked to the McKinley sequence, a series of plutons thought to have been emplaced at about 55 Ma.(1)².

²-Underlined numbers in parentheses refer to the list of references at the end of this report.

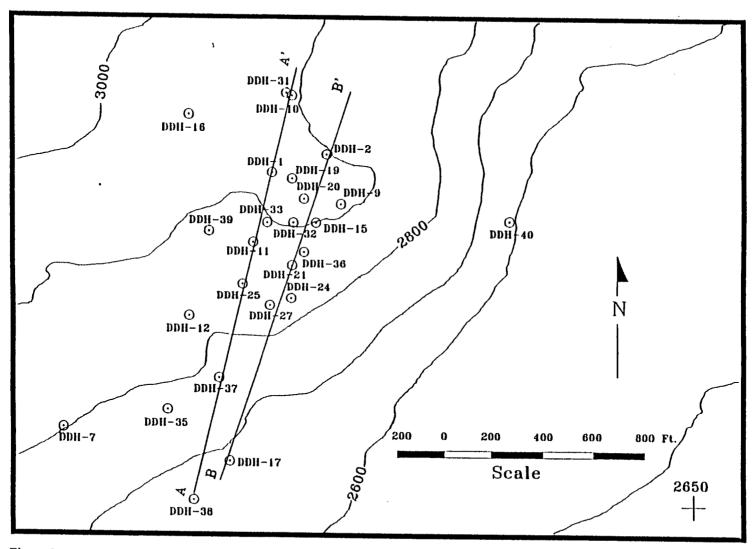


Figure 2. - Drill hole and cross section location map.

In 1982, a drilling project conducted by Billiton Exploration USA resulted in the discovery of a tin-bearing sheeted vein system, with a reported geologically indicated resource of 5 million metric tons with an average grade of 0.2 percent tin (2).

The Coal Creek tin prospect was investigated during brief reconnaissance in the summers of 1984, and 1988 by the U.S. Bureau of Mines(3). The investigations included geologic mapping, sample collection and analyses. Core from four diamond drill holes was shipped to the Bureau's Salt Lake City Research Center for mineral beneficiation testing. The results were reported by Johnson and Parker (4).

REGIONAL GEOLOGICAL SETTING

The Alaska Range batholith is part of the Talkeetna superterrane which is believed to have been accreted to the continental margin of stable Alaska in the Paleocene (5). The northern plutons of the Alaska Range batholith are known as the McKinley sequence (6). The Coal Creek granite is part of the McKinley sequence plutons which intrude Paleozoic and Mesozoic sedimentary and volcanic rocks.

Strontium and oxygen isotopic evidence suggest the source for the Coal Creek granite was influenced by sedimentary crustal material (5). Lead isotopes can also be used as an indicator of granite source material (7). Lead isotope ratios measured on a potassium feldspar collected from the Coal Creek granite implies that it was emplaced in a continental margin setting, incorporating lead from both an igneous and sedimentary source (table 1). The sulfur isotope values for the Coal Creek granite are negative (table 1), and can be best explained by the incorporation of some light biogenic sulfur from continental crust (8) and/or oxidation of a reduced fluid (9). Values of lead and sulfur isotopic ratios measured on the Mesozoic flysch in the Coal Creek area, identified by Lanphere and Reed (5) as the most likely contaminant, are sufficiently different from those seen at Coal Creek to suggest that these sediments constitute a small fraction of the source (table 1).

Table 1. -Available isotope data from Coal Creek and vicinity

Rock Type	²⁰⁶ Pb/ ²⁰⁴ Pb	207РЬ/204РЪ	²⁰⁸ Pb/ ²⁰⁴ Pb	δ ³⁴ S
Granite	19.030	15.551	38.386	-7.9
Skarn	_			-5.4
Flysch	22.683	15.879	38.893	-34.6

Biotites from McKinley sequence plutons have been dated at 55 to 57 Ma.(5). Biotite from the younger Coal Creek granite has yielded a K/Ar date of 49 +/- 2.5 Ma. This is evidence that the tin related magma crystallized slightly later than the main plutonic event.

LOCAL GEOLOGY

The following sections describe the petrology, mineralogy and geochemistry at Coal Creek. Because there is limited surface exposure at Coal Creek the bulk of the data is derived from rock samples taken from the drill core.

Igneous Petrology

The Coal Creek prospect granite consists of two texturally and chemically different units: (1.) a seriate granite porphyry, which is intruded at depth by (2.) a fine-grained equigranular to slightly porphyritic granite.

The seriate granite outcrops at the surface and forms a small resistant knob on the flank of a hillside. This unit contacts Devonian metasediments locally, producing hornfels and skarn. The fine-grained granite lies below the seriate granite. Its only surface expression is 0.5 to 1 m thick aplitic granite dikes. At the contact between the two major units is a 1-3 meter zone of crenulate and dendritic layers. This texture has been recognized at the Henderson porphyry molybdenum deposit in Colorado, and described as unidirectional solidification textures which are useful for interpreting contacts and timing relationships between intrusive units (10). World-wide, they commonly occur as multilayer sequences in the apical and marginal parts of igneous intrusions. At Coal Creek these layers consist of pegmatitic quartz, potassium feldspar, and biotite dendrites mixed with aplitic granites. Throughout the rest of this paper this unit will be referred to as the pegmatite unit.

Greisen alteration is the main alteration type at Coal Creek. It is characterized by complete quartz flooding and destruction of the original igneous fabric. Other associated minerals include white mica, tourmaline, topaz, fluorite, pyrrhotite, cassiterite, sphalerite, arsenopyrite, pyrite, and chalcopyrite. The most intense alteration is located in the central portion of the seriate granite (fig. 3).

Major-Minor Element Geochemistry

The whole rock major oxide analytical results for all Coal Creek granitic units indicate that they are high in silica, alkalis and aluminum and low in titanium. Major oxide chemistry is not an effective means of differentiating between the three textural units because of their similar compositions. The major oxide content and normative calculations indicate that all the granitic units are very evolved with differentiation indices (D.I. = sum of normative quartz + orthoclase + albite) ranging from 91 to 97 (table 2). The data for the Ruth Pluton taken from Lanphere and Reed (5), which is a related granite in the vicinity of the deposit is included for comparison. All of the Coal Creek samples are peraluminous ($Al_2O_3 > K_2O + Na_2O + CaO$) and all but one contain normative corundum (table 3). The high D.I. and slightly peraluminous nature is similar to other granite related tin deposits in Alaska (11, 12, 13). The three Coal Creek textural units and the Ruth pluton can be discriminated on plots of trace element content versus D.I. (fig. 4). The pegmatite unit plots intermediate to within the fine-grained granite field and may represent a composition similar to that of the fine-grained unit. The plots display progressive fractionation from the Ruth pluton granites, to the seriate, to the most evolved, fine-grained, Coal Creek granite.

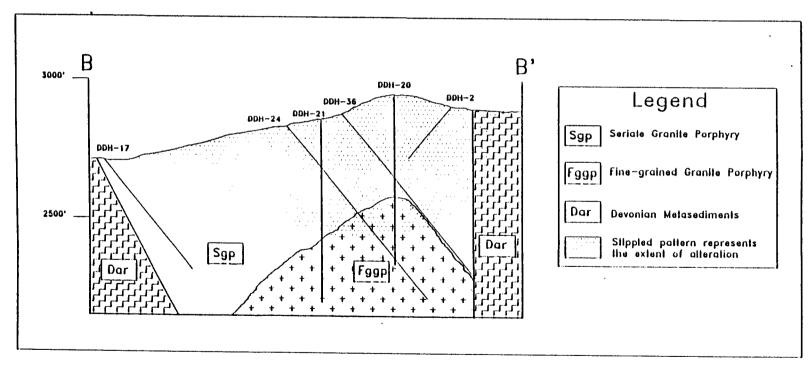


Figure 3. -- N15E cross section showing the extent of alteration with a stippled pattern.

Table 2. -- Major element oxides and minor element analyses for Coal Creek and the Ruth Pluton

Rock Type	6	ate Gra orphyr			F	Pegmati	te Zone	3		F	ine-Gra	ined G	ranite l	Porphyi	ry	Ruth Pluton*					
Sample Number ^{\3}	20-250	21-380	24-380	20- 390A	20- 390B	21- 450A	21- 450B	24- 400A	24- 400B	20-480	21-550	24-510	20-590	21-640	24-760	70AR- 116	76AR- 20	76AR- 19	70AR-	76AR-	76AR-
SiO ₂ \I	73.20	72.50	74.30	73.60	73.00	75.40	73,20	74.70	75.80	73.00	74.80	73.30	74.10	73.50	74.40	74.70	73.50	75.10	68.60	22.40	
Al ₂ O ₃	13.80	13.40	13.10	13.00	12.60	13.30	13.10	12.20	11.80	13.20	12.90	13.40	12.80	13.20	12.50	13.30				72.40	76.00
Fe ₂ O ₃	0.75	0.42	0.38	0.43	1.66	0.15	0.26	0.41	0.46	0.41	0.13	0.34	0.51	0.16	0.29		13.80	13.10	15.30	14.40	13.20
FeO	1.02	0.74	1.02	0.80	0.74	0.89	0.89	1.15	1.15	1.15	1.15	0.96	0.77			0.10	0.20	0.70	0.56	0.52	0.30
MgO .	0.10	0.07	0.05	0.05	0.08	0.03	0.05	0.04	0.04	0.05	0.02	0.03	0.77	0.96	1.08	1.60	1.90	0.84	2.40	1.80	0.84
CaO	1.25	0.79	0.67	0.57	0.66	0.42	0.58	0.44	0.47	0.41	0.29	0.32	0.43	: 0.05	0.06	0.15	0.27	0.32	1.10	0.28	0.07
Na ₂ O	3.89	4.33	3.48	3.62	3.69	4.42	4.39	3.29	3.20	3.43	4.10	4.15		0.40	0.54	1.20	1.40	1.30	2.40	2.10	0.77
K ₂ O	4.32	4.43	5.00	5.21	5.30	4.86	4.88	5.22	5.11	5.00			4.18	4.10	3.95	3.10	2.80	3.10	3.40	3.20	3.40
TiO,	0.08	0.06	0.01	0.14	0.31	0.02	0.07	0.01			4.29	4.59	4.22	4.48	4.33	4.70	4.70	4.80	4.40	* 4.10	4.90
P ₂ O ₅	0.34	0.05	0.27	0.17	0.28				0.04	0.03	0.02	0.01	0.10	0.03	0.12	0.18	0.37	0.17	0.50	0.40	0.07
MnO	0.03	0.03	0.15	0.03	0.28	0.11	0.17	0.19	0.25	0.09	0.16	0.15	0.17	0.23	0.29	0.04	0.10	0.11	0.17	0.14	0.08
LOI	0.61	0.46	0.55	0.55	0.03	0.04 0.37	0.04	0.09	0.07	0.07	0.05	0.04	0.06	0.06	80.0	0.06	0.02	0.02	80.0	0.03	0.02
Totals	99.39	97.28	98.98	98.17	98.72	100.01	0.23	0.42	0.33	0.76	0.19	0.28	0.56	0.24	0.34	-	•	-	•	•	-
	<20	<20	⊘ 0.70	<20			97.86	98.16	98.72	97.60	98.10	97.57	97.94	97.41	97.98	99.13	99.06	99.56	98.91	99.37	99.65
Ba ¹² Nb	17	18	15		<20	<20	<20	<20	<20	<20	<20	<20	<20	<20	<20	800	1300	780	1100	1900	385
Rb	320	310	550	24	31	23	27	19	26	27	34	38	37	37	34	29	22	20	22	20	24
Sı				495	520	555	500	525	500	870	840	755	790	880	845	229	179	158	126	99	245
Zr	ব	ব	ব	<3	ধ	<5	<5	ব	<	⋖	ব	ধ	্	ধ	ব	69	119	87	346	217	47
Y	27	39	32	21	16	18	18	23	19	15	12	16	26	16	13	160	220	120	190	250	92
•	ব	ধ	ব	42	39	35	43	23	38	48	54	81	54	60	40	50	36	39	16	40	86
S	0.05	0.02	0.14	0.02	0.02	0.02	0.02	0.12	0.14	0.02	0.02	0.02	0.02	0.02	0.03				-	-	
Zo	. 311	84	185	141	129	63	63	301	282	178	63	78	42	63	65	60	71	42	50	55	44
a	200	200	200	200	200	200	200	200	200	200	50	50	200	200	740	50	90	40	80	80	30
F	3080	1142	4330	1331	1181	2060	2454	2480	2628	5780	4820	4850	4030	4375	3672	1200	700	600	500	500	900
и	148	142	549	203	209	302	321	258	252	712	618	385	686	734	742	150	140	91	81		
Sn	21	9	39	20	15	5	11	175	160	22	5	22	25	9	23	9	4	4	81	84	170

^{*}Ruth Pluton data from Lanphere and Reed (1985)

Major element oxides reported as weight percents

¹² Minor elements reported as ppm

^{\3} Sample numbers are defined as, drill hole number-intercept depth; reference cross sections in figures 3 and 5.

⁻ Not analyzed

Table 3. --CIPW normative minerals from Coal Creek and the Ruth Pluton

Rock Type	3	ate Gra orphyr			F	egmati	te Zone)		Fine-Grained Granite Porphyry			Ruth Pluton*								
Sample Number ^{\1}	20-250	21-380	24-380	20- 390A	20 ₁ 390B	21- 450A	21- 450B	24- 400A	24- 400B	20-480	21-550	24-510	20-590	21-640	24-760	70AR- 116	76AR- 20	76AR- 19	70AR-	76AR-	76AR-
Q Or Ab Aa C Hy Mi Ii Ap Hm Di En Fs	32.01 25.83 33.34 4.08 1.26 1.44 1.10 0.15 0.79	29.17 27.07 37.82 3.74 0.16 1.17 0.62 0.11 0.12	33.84 30.02 29.95 1.61 1.40 1.98 0.55 0.02 0.63	32.09 31.56 31.39 1.77 0.79 1.09 0.64 0.27 0.39	31.02 31.85 31.73 1.49 0.26 0.20 1.59 0.61 0.65 0.60	29.82 28.84 37.57 1.37 0.26 1.63 0.22 0.04 0.25	28.20 29.55 38.08 1.65 1.46 0.39 0.13 0.39	35.00 31.56 28.52 0.99 0.79 2.07 0.61 0.02 0.44	37.06 30.67 27.50 0.75 0.75 1.92 0.68 0.08	33.45 30.49 29.95 1.50 1.67 2.04 0.62 0.06 0.21	34.08 25.88 35.45 0.44 1.38 2.14 0.20 0.04 0.37	31.39 27.89 36.13 0.66 1.40 1.66 0.51 0.02	33.60 25.59 36.30 1.07 1.00 1.06 0.77 0.19 0.39	32.38 27.24 35.71 0.47 1.48 1.86 0.25 0.06 0.56	34.47 26.18 34.27 0.77 1.06 1.89 0.43 0.23 0.70	35.09 28.04 26.49 5.75 1.04 	35.26 28.03 23.91 6.16 1.89 - 0.29 0.71 0.24 -	35.62 28.48 26.34 5.63 0.75 - 1.02 0.32 0.26 -	24.46 26.28 29.08 10.91 1.00 	32.79 24.37 27.24 9.43 1.27 0.76 0.76 0.33 0.70 2.28	35.58 29 05 28.86 3.12 1.17 0.44 0.13 0.19
Plagis An Pl *Ruth Plutor	91.18 - 91.18	9 94.06	5 93 81	95.04	4 94.60	4 96.23	4 95 83	3 95.08	3 95 23	5 93 89	l 95.41	2 95.41	3 95 49	1 95 33	94.92	17 89 62	0 07 20 87.19	0 05 17 90 44	26 79 83	0 05 25 84.41	93.4

^{*}Ruth Pluton data from Lanphere and Reed (1985)
\1 Sample numbers are defined as, drill hole number-intercept depth; reference cross sections in figures 3 and 5.

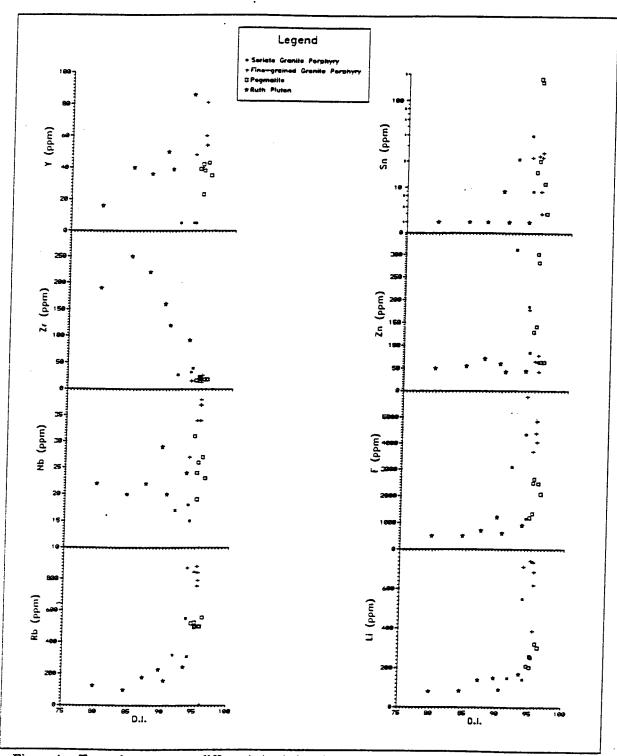


Figure 4. --Trace element versus differentiation index plots.

Granite Mineralogy

Feldspars

Potassium feldspar is the most abundant feldspar. In the seriate granite unit it is subhedral to euhedral and ranges in length from 0.5-3.0 cm. It is generally perthitic with individual albite perthites reaching 0.2 cm in size. In the fine-grained granite unit the potassium feldspar is subhedral to anhedral and 0.2 cm in length. In the pegmatite unit it occurs as dendrites and euhedral crystals that can reach 20 cm. The potassium feldspar is usually altered to fine-grained clays or sericite, and in some samples it takes on a brown color.

Plagioclase is strongly altered and only a few primary grains remain. They are albite rich with "An" contents of 1-5 %. The plagioclase is altered to clays or replaced by silica in the silicified zones.

Micas

Three mica minerals were identified. The sericite is a fine-grained alteration product of the feldspars and topaz. The sericites have low iron, fluorine, and chlorine contents which help distinguish them from the other coarse-grained white mica.

The biotites are end member siderophyllites, with high fluorine and chlorine contents. Biotites are scarce in both the seriate and fine-grained unit. In the pegmatite, biotite forms 20-40 cm layers of biotite dendrites in a quartz, potassium feldspar matrix. Individual biotite dendrites may reach 10 cm.

The coarse-grained white micas are most abundant. They are located near veins and in the areas most affected by the silicic and greisen alteration. The white micas have the highest fluorine contents with an average of 5 wt.%. Based on their very high iron content they are zinnwaldite, which is a common lithium-bearing white mica associated with tin deposits. Lithium can not be detected with an electron microprobe, but the whole rock data indicates high lithium contents, and micas are the likely host.

Quartz

Quartz is abundant in all units. It forms 1 cm euhedral phenocrysts in both the fine-grained and seriate units. It also occurs as fine anhedral grains in the silicified areas. In the pegmatite unit it is subhedral to anhedral and forms as open space fillings.

Alteration Minerals

Tourmaline is a common alteration mineral. It occurs in veins and pods in the areas most affected by greisen and silicic alteration. Colors range from brown to blue. The variation in color is probably due to small differences titanium content.

Topaz is associated with the open spaced veins related to mineralization. It is subhedral to euhedral and difficult to distinguish from quartz. Topaz contains fluorine and is commonly associated with fluorite, both of which suggest high fluorine concentrations in the hydrothermal fluid during mineralization.

Ore Mineralogy

The ore minerals are concentrated in near vertical 0.5-2.0 cm open-spaced quartz, topaz, and tourmaline veins with up to 15 cm silicic envelopes. Within these envelopes the primary igneous texture is destroyed. The vein envelopes are commonly vuggy and contain tourmaline, cassiterite and sulfides. The open-spaced veins are late and crosscut all other vein types. These veins are concentrated in the upper seriate granite and appear to be rooted in the equigranular granite, as they can only be traced 10-20 m below the seriate-equigranular granite contact.

There are a variety of sulfide, and oxide minerals associated with the mineralization at Coal Creek. The most important are cassiterite, stannite, sphalerite, arsenopyrite, pyrrhotite, pyrite, marcasite, loellingite, bismuthinite, chalcopyrite, and galena. This mineral assemblage indicates a low sulfidation and oxidation state during mineralization.

Cassiterite is the dominant tin-bearing mineral, however, petrographic and electron microprobe study of the sulfide mineral assemblage shows that stannite represents approximately 3 percent of the total tin-bearing minerals. The bulk of the silver is contained in the stannite and in the 2-5 micron galena grains. This is important to the deposit's ultimate economic potential because a small amount of the tin, but a large portion of the silver may be difficult to extract.

Sulfidation state and temperatures of formations were obtained using the composition of coexisting mineral pairs. Sulfide mineral compositions were determined using an electron microprobe (table 4). Three different mineral pairs and methods were used to test for variation within the system and between the methods.

The compositions of coexisting pairs of arsenopyrite and sphalerite indicate temperatures of formation of 412-496°C (table 5). Similar values were calculated using arsenopyrite-loellingite-pyrrhotite mineral stability. Coexisting sphalerite and stannite pairs indicate temperatures of formation of 287-388°C (table 6). Therefore the stannites probably crystallized at lower temperatures than the arsenopyrite, loellingite and sphalerite. The observation that stannite normally rims sphalerite also supports this hypothesis.

The arsenopyrite-sphalerite temperature contours were plotted on the cross section A-A' (fig 5). They indicate a trend of increasing ore mineral crystallization temperature with distance from the fine-grained unit. This interesting inwardly decreasing trend for ore mineral crystallization temperature was supported by all three geothermometers, although much more data is needed to confirm this pattern.

CONCLUSIONS

The Coal Creek prospect consist of a seriate granite porphyry that is intruded at depth by a fine-grained granite porphyry. The two greisen-altered granites intrude Devonian metasediments locally producing hornfels and skarn. At the contact between the two units is a 1-3 meter zone of UST's. The whole rock geochemistry indicates that the granite units are slightly peraluminous, extremely fractionated granites.

The mineralization and greisen alteration is centered in the upper seriate unit. The majority of the ore minerals are located in near vertical 0.5 to 2.0 cm open-spaced quartz veins and their associated greisen alteration envelopes. Cassiterite and stannite are the two tin-bearing minerals present at Coal Creek. The stannite is important because

Table 4. —Chemical compositions of coexisting mineral pairs determined with the electron microprobe

Sample #	\1	As*	S	Zn	Cu	Fe	Mn	Ag	Cd	Sn	Tot.
17-400	SI-I	0.00	32.03	1.88	26.66	15.18	0.01	0.14	0.00	25.56	101.46
17-400	Sp-1	0.00	34.59	45.97	0.10	15.64	2,51	0.00	0.47	0.03	99.32
17-400	St-2	0.00	29.92	7.12	24.42	13.54	0.07	0.16	0.07	22.75	98.05
17-400	Sp-2	1.49	34.59	47.34	0.15	14.91	2.55	0.05	0.31	0.00	101.39
17-400	St-3	0.20	29.00	7.67	23.73	13.19	0.10	0.08	0.01	21.74	95.73
17-400	Sp-3	0.13	34.43	47.11	0.13	15.11	2.44	0.01	0.38	0.00	99.75
17-400	St-4	0.00	29.27	3.24	26.68	12.45	0.03	0.20	0.07	25.20	97.13
17-400	Sp-4	0.00	34.41	48.83	0.10	13.67	1.94	0.04	0.37	0.00	99.37
25-522	St-1	0.35	30.15	1.56	28.43	13.36	0.01	0.34	0.01	25.82	100.03
25-522	Sp-1	0.00	33.97	49.3	0.32	13.27	1.18	0.00	0.46	0.01	98.51
25-522	St-2	0.18	29.86	1.67	28,42	12.33	0.02	0.24	0.04	24.79	97.56
25-522	Sp-2	0.07	34.2	49.47	0.24	13.59	1.06	0.00	0.50	0.00	99.13
25-346	St-1	0.00	29.95	5.51	26.02	12.65	0.08	0.25	0.05	24.26	98.77
25-346	Sp-I	0.00	33.3	47.8	0.13	14.09	1.72	0.01	0.41	9.02	97.49
25-566	St-1	0.46	30.1	1.45	28.34	12.71	0.04	0.37	0.00	27.32	100.8
25-566	Sp-1	0.07	33.95	47.22	0.25	14.84	1.90	0.24	0.43	0.00	98.91
25-566	St-2	0.00	29.03	1.82	28.19	12.78	0.02	0.19	0.00	25.85	97.89
25-566	Sp-2	0.00	33.66	45.00	0.07	15.10	2.63	0.00	0.53	0.01	97.00
25-566	St-3	0.00	29.58	3.71	27.20	13.66	0.13	0.35	0.05	25.34	100.03
25-566	Sp-3	0.00	33.90	47.06	0.10	14.60	2.41	0.00	0.41	0.00	98.48
25-346A	St-1	0.59	29.63	1.80	28.01	12.96	0.03	0.21	0.00	26.70	99.94
25-346A	Sp-I	0.00	34.01	47.62	0.23	14.02	1.69	0.00	0.43	0.02	98.01

Sample #		As	S	Zn	Cu	Fe	Mn	Ag	Cđ	Sn	Tot.
25-380	asp-l	47.95	19.41	0.00	0.00	34.82	0.00	0.00	0.00	0.01	102.19
25-380	sp-l	0.26	33.78	46.27	0.15	15.10	1.73	0.08	0.34	0.00	97.71
25-380	аяр-2	47.43	20.31	0.16	0.00	35.23	0.01	0.00	0.00	0.01	103.15
25-380	50-2	0.21	34.03	48.12	0.16	14.35	1.64	0.00	0.52	0.00	99.03
25-380	2sp-3	45.46	20.18	0.04	0.00	35.03	0.03	0.00	0.02	0.02	100.78
25-380	50-3	0.21	34.03	48.12	0.16	14.35	1.64	0.00	0.52	0.00	99.03
25-380	авр-4	47.35	19.56	0.03	0.01	34.92	0.00	0.02	0.00	0.00	101.89
25-380	sp-4	1.38	34.05	48.01	0.11	14.24	1.31	0.00	0.45	0.04	99.59
25-500	asp-i	44.33	18.67	2.74	0.00	33.88	0.07	0.00	0.00	0.00	99.69
25-500	50-l	0.00	33.75	47.77	0.06	14.68	1.85	0.06	0.41	0.09	98,67
25-500	150-2	48.89	17.81	0.03	0.00	34,43	0.01	0.00	0.07	0.02	101.26
25-500	sp-2	0.00	34.26	44.34	0.13	16.11	2.20	0.00	0.52	0.02	97.58
25-346A	asp-i	52.76	16.54	0.00	0.00	33.27	0.03	0.00	0.01	0.01	102.62
25-346A	sp-l	0.28	33.86	46.58	0.11	14.81	1.96	0.00	0.42	0.00	98.02

Sample #		As	S	Zn	Cu	Fe	Mn	Ag	Cd	Sn	Tot.
25-346A 25-346A	lo-2 350-2	70.60 48.39	2.15 17.67	0.02 0.01	0.01	28.97 34.13	0.00	0.03 0.08	0.00	0. 00 0. 00	101.78
2 5-522 25-522	lo-i asp-i	71.09 47.33	1.75 18.99	0.02 0.00	0. 00 0. 00	28.71 34.52	0.02 0.01	0.00 0.04	0.00 0.05	0 .00 0.05	101.59

^{*}All elements reported as weight percent

^{\1} Sample numbers are defined as, drill hole number-intercept depth; reference cross sections in figures 3 and 5.

st. Represents stannite

sp. Represents sphalerite

asp. Represents arsenopyrite

lo. Represents loellingite

Table 5. –Temperatures derived from coexisting sphalerite and arsenopyrite in degrees C. The geothermometer from Scott and Barnes $(\underline{14})$

Sample #	As	Zn	Temp
25-380-1	34.2	72	496
25-380-2	33.3	74	460
25-380-3	32.5	75	426
25-380-4	33.8	74	479
25-500-1	32.4	74	412
36-625-1	33.0	72	428
36-625-2	32.8	72	417

As: Atomic percent arsenic in arsenopyrite

Zn: $[(X_{Zn} \text{ in sphalerite})/(X_{Zn} + X_{Fe} \text{ in sphalerite}) \times 100]$

Table 6. —Temperatures derived using the stannite-sphalerite geothermometer of Shimizu and Shikazono (15)

Sample #	I	П	Temp.
17 400 1	0.42	0.20	201
17-400-1	9.43	0.39	301
17-400-2	2.22	0.37	381
17-400-3	2.01	0.37	388
17-400-4	4.49	0.33	331
25-522-1	10.01	0.32	287
25-522-2	8.65	0.32	295
25-346-1	2.68	0.35	365
25-566-1	10.25	0.37	293
25-566-2	8.23	0.39	308
25-566-3	4.31	0.36	339
25-346A-1	8.44	0.34	300

I: (X_{Stannite}/X_{Kesterite}) in Stannite

II: (X_{Pyrrhotite}/X_{Sphalerite}) in Sphalerite

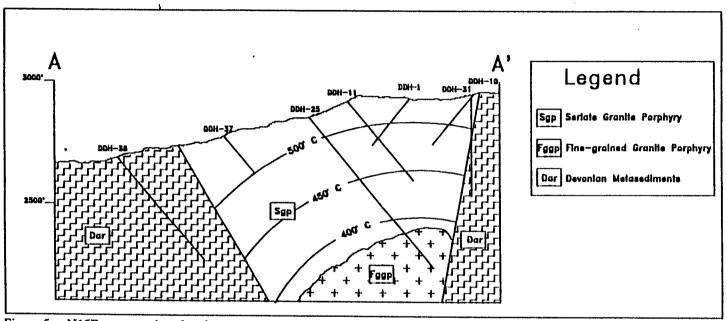


Figure 5. --N15E cross section showing temperature contours derived from coexisting arsenopyrite, sphalerite, mineral pairs

although it contains a small portion of the total tin, it contains a significant portion of the silver. Silver is also hosted by 2 to 5 micron argentiferous galena grains. The alteration and ore mineralogy suggest that the mineralizing fluids were enriched in F, B, Li, and Cl. The ore mineralogy also indicates a low oxidation and sulfidation state, and crystallization temperature range of 300 to 500° C.

The genetic origin of the tin mineralization is interpreted from petrographic observations and a collection of trace and major element concentration data from the different igneous rock types at Coal Creek and vicinity. These interpretations combine to form a rational basis for relating the distribution of hydrothermal mineralization to the igneous host lithologies. Exploration criteria and limiting constraints on the potential size of this type of tin deposit can be gleaned from this data.

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APPENDIXES

Appendix A. Drill hole data from the summer 1982 drilling project at Coal Creek.

Hole Number	Depth of Hole	Bearing	Dip	Coordinates
	99-889 (*)	gaboutan owner, tearner one could	Midnographic	
1	248.4 250.3	S15W	50	N10167,E9698
	201.6	S15W S70E	50 60	N10118,E9892
4	196.6	S70E	50 50	N10859,E9436
5.00	201.7	5/0E	50	N8238,E9485 N4840,E8745
6	160.2	N70W	50	N7934.E6710
7	248.2	S70E	50	N8980,E6770
8 - Committee Home Committee		6000000000000 <u>0000000</u> 00000000	Vii totatata e e e e e e e e e e e e e e e e e	
9 10	158.9	NISE	50:	N9883,E9917
îi	270.0 405.0	S1SE	50	N10368.E9746
12	874.0	NISE NISE	50:	N9784,E9603
13	196.0	S45E	50 50:	N9444.E9317
14	376.0	S83W	70	N12230,E12207 N6196,E5894
15	570.0	0::	90	N9828,E9840
16	866.0	S1 <i>5</i> E	70	N10265,E9312
17				
18 19	693_3	0:	90	NI MAT EDIZA
20	609.8	0	90	N10001,E9740 N9915,E9790
21	653.8:	o.	90	N9656.E9740
22	555.4	0	90	N9484.E9640
23	692.8	0	90	N9915.E10090
24	803.2	N15E	50	N9539,E9735
25	800.3	N15E:	50	N9588,E9552
26	206.3	0	90	N8768,E6881
27 28	172.8	0:	90%	N8322,E7017
28 29	91.6	0	90	N8579,E7589
30	295.7 133.7	0>	90:	N11418,E11055
31:	418.5	0 0:	90	N10883.E10492
32	727.5	0	90	N10373,E9741
33	746.9	a.	90 90	N9828,E9740 N9828,E9640
34	593.0	0	90	N10001,E9940
35	500.7	N15E	50:	N9054,E9214
36	762.8	NISE	50	N9732.E9794
37	194.3	N15E	50	N9200,E9454
38	547.2	N15E	50	N8725,9309
39:	645.4	N15E	50	N9831,E9403
40	237.4	N15E	<i>5</i> 0	N9828,E10626
41	215.1	N3SE	50::	N12254,E11729
42	172.0	N3SE	50	N12493,11691

Appendix B. Available interval and assay data from the summer 1982 drilling project at Coal Creek.

DDH	FROM (ft.)	TO (ft.)	RECOVERY (ft.)	Sn (ppm)	Ag (ppm)
19	5	10	35	2100	19.0
19 19	10	20	9.3	105	3.8
19	20 28	28 37	8.4 9.0	47	3.3
19	37	47	10.0	390 500	5.1 2.6
19	47	57	10.0	280	2.5
19 19	57 63	63	6.0	620	8.3
19	63 71	71 78	7.7 6.4	1480 140	14.0
19	7 8	88	8.0	1000	4,0 8.0
19	88	98	8.2	180	4:1
19 19	98 108	108	8.4	2053	0.7
19	115	115 125	6:1 8.8	110 32	6.1
19	125	135	75	32 160	2.4 4.4
19	135	145	9.8	820	6.3
19 19	145 154	154 164	8.9	90	4.2
19	164	174	9.8 9.9	1500 25:	4.4
19	174	179	5.0	1000	1.3 11.0
19	179	189	9.9	1000	21
19 19	189 19 9	199 207	9.5	1804	0.7
19	207	213	7.9 5.9	135 535	2.4
19	213	220.	7.0	830°	18.0 2.8
19	220	225	4.9	80	4.8
19 19	., 21 23	235 245	9.8	475	3.1
19	245	253.	10.0 7.9	36 5	5.8 0.4
19	253	261	8.0	595	8.1
19 19	261	271	10.0	1070	22.
19	271 281	281 290	9.9 9. 0	19	9.2
19	290	300	9.4	3150 1750	کـ6 9.2
19	300	309	8.0	1000	9.9
19 19	309	319	10.0	390	2.0
19	319 329	329 339	10.0	3175	9.2
19	339	350	10.0 10.9	4000 3250	6.3 25.0
19	350	360	9.6	315	1.1
19 10	360 370	- 370	9.6	2300	3.5
19 19	370 380	380 391	9.1 9.9	28	1.0
19	391	401	9.7	330 57	1.4 1.2
19	401	411	93	5	0.5
19 19	411 421	421 428	9.3	12 13	0.4
19	428	428 438	6.8 9.2	770	0.4
19		448	10.0	100	3.6 0.4

DDH	FROM (ft.)	TO (ft.)	RECOVERY (ft.) Sn (ppm)	Ag (ppm)
19	448	458	9.8	65	0.4
19	458	468	9.8	295	1.8
19	468	478	9.7	225	7.5
19	478	488	9.5	6000	7.5
19	488	498	9.7	2200	
19	498	508	9.8	225	2.6 0.8
19	508	518	9.8	2400	8.0
19	518	528	9.9	4360	16.0
19	528	538	10.0	415	1.2
19	538	548	10.0	175	2.4
19	548	553	5.0	28	0.4
1 9	553	563	9:9	2700	2.0
19 19	563 573	573 583	10.0 10.0	210	0.3
19 19	583	593	9.9	713 195	0.3: 0.2
19	593	603	10.0°	87	0.2:
	603	613	10.0	660	2.6
19	613	623	10.0	1000	1.9
19	623	633	10.0	41	0.2
19	633	643	10.0	365	0.3
19	643	653	10.0	215	0.2
19	653	663	10.0	29°	0.2
19	663	673	10.0	26	
19	673.	683.	10.0	62.	0.2
19	683	693	10.3		0.2
20:::	0	8	7.8	77 9	0.2 5.8
20	8	17	8.8	160	6.6
20	17	27	9.7	19 5	1.4
20	27	37	9.4	205	2.4
20	37	4 7	9.6	5 45	1.5
20	47	52	5.0	3450	3.6
20	5 Z :	59	7.0	2320:	3.5
20	59	69	9.8	210	2.0
20	69	79	9.8	2590	7.4
20	79	87	7.9	3000	2.6
20:	8 7	9 7	9.8	385	
20	97	107	9.8	1800	1.0 1.8
20	107	117	9.6	6 300 :	14.0
20	117	127	7.8	7350	20.0
20	127	137:	7.5	500:	2.7
20	137	147	9.7	210	1.4
20:	147:	157	9. 8	185	29:
20	157	167	8.5	3050	22
20	167	177	9:4	3900	1.4
20	177	187	8.9	1800	2.9
20:	187:	197	8.9°	5700	45
20	197	207	8.6	2200	
20° 20	207	217	8.2	1900	3.2 5.3
20:	217	222	4.6	3860	3.1
	222	232	9.5	110:	1.4
20	232	2A2	9.8	380	0.9
20	2 42	252	9.8%	820:	0.6
20	252	262	9.4	4360	كة
20:	26 2	272	9.5	615:	32.
20	272	282	9.8	600	6.0
20:	28 2	293	10.8	690	2.6
20	293	303	9.8	4200	9.2
20	303	313	9.8	325	4.0
20	313	323	10.0	110	1.6

DDH	FROM (ft.)	TO (ft.)	RECOVERY (ft.)	Sn (ppm)	Ag (ppm)
20	323	. 333	10.0	3800	6.6
20	333	343	10.0	530	3.3
20 20	343 353	353 363	9.9 9.9	29 1400	0.8 3.7
20	363	373 383	10.0	32	0.6
20 20	373 383	393	10.0 9.8	1200 8500	4.0 35.0
20 20	393 403	403 413	9.4	125	0.5
20	403 413	413 423	9.2 8.9	2700: 140	18.0 0.7
20 20	4 23 433	433 443	9.5 9.8	38 210	0.2
20	443	433	9.8	210 220	0.6 2.9
20 20	453 463	463 473	9.5 10.0	1900 725	12.0 11.0
20	473	483	10.0	2750	0.5
20 21	483 10	487 20	43 93	550 29	3.3 1.7
21	20	30	93	26	0.9
21 21	30 40	40 50	9.7 9.7	77 165	0.7 0.4
21	50	60	9.9	21	1.4
21 21	60 70	70 80	9.8 9.9	26 54	1.0 0.8
21 21	80	90	10.0	46	2.8
21 21	90 100	100 110	10.0 1 0.0	43 11	3.7 0.7
21	110	120	9.8	13	1.8
21: 21	120 130	130 140	9.8 9.7	32. 26	3.6 9.0
21:	140	150	9.6	15.	2.4
21 21	150 160	160 170	9.6 9.1	22 11	1.5 0.8
21	170	180	9.4	9	1.7
21 21	180 190	190 200	83 63	360 134	13 45
21	200	210	7.0	35	1.4:
21 21	210 220	220 230	8.6 9.2	20 8 2 :	1.2 1.5
21	230	240 250	9.3	42	0.9
21 21	240 250	250 260	9.6 9.8	27 54	0.8 1.9
21 21	250 270	270 280	10.1	25:	0.5
21	270 280	290 290	10.0 9.8	57 11	1.3 0.5
21 21	290 300	300 310	9.6 9.8	175	1.1
21	310	320	8.1	430 155	2.5 3.1
21 21	320 330	330 340	9,4 0.6	155 100	6.5
21	340	350	9.6 9.4	200 800	4.9 9.0
21 21	350 360	360 370	9.7 8.1	740 2000	2.6 17.0
21	370	380	7.2	28 440	1.6
21 21	380 390	390 400	9.6 9.5	440 1100	2.9 0.4
21	400	410	8.8	30	0.6
21 21	410 420	420 430	10.3 9.8	5 11	0.4 0.5

DDH	FROM (ft.)	TO (ft.)	RECOVERY (ft.)	Sn (ppm)	Ag (ppm)
			20		0.4
21	430	440	9.9	6	0.4
21	440	450	9.9	6	0.6
21	450	460	9.9	5	0.4
21	460	470	9.7	19	0.4
21	470	480	9.7	66	0.5
21	480	490	9.9	31	0.2
21	490	500	8.8	69	0.2
21	500	510	9.0	270:	0.4
21	510	520	9.0	11	0.2
21	520	530	9.7	18:	0.2
21	530	540	9.8	12	0.2
21	540	550	9.8	7	0.2
21	550	560	10.0	22	0.4
21.	560	570	10.0	1 2	0.2.
21	570	580	10.0	17	0.3
21	580	590	9.9	9:	0.2
21	590	600	9.9	3600	0.5
21	600	610	9.7	1800	0.3
21	610	620	9.8	855	0.2
21	620	630	9.9	38:	0.2
21	630	635	4.9	105	0.4
21	635	645	9.2	700:	0.6
21	645	653	6.3	13	0.2
22::	10	20:	10.0	85	0.6
22:	20	30	9.5	125	1.3
72	30	40	9.6	500	2.0
22	40	50	9.9	26	0.6
22::	50	60	9.9	68	1.5
22.	60	70	9.8	780	1.4
22.	70	8 0 :-	9.8:	61	0.4
22	80	90	9.7	41	0.6
22	90:	100	9.9	27	0.4
22	100	105	4.8	70	0.4
22	105		9:7	205:	0.7
22,	115	115 125	10.0	16	0.6
22	125	135	9 .9	32	1.1
22	135	140	4.5	13	0.4
2 2 .	140	151	73	30:	0.9
22.	151	161	4.7	110	0.3
22:::	161	169	7.5. 9.6	95 19	0.4 1.0
22 22	169 179	179 189	7.4	45	22
22	189	199	7.4	45	1.7
22	199	2 09	8.4	70	4.2.
22	209	219	9.5	45	6.7
22:::	219	229	9.7	31	0.9
22	229	239	کـ8	34 25:	1.2 1.2
22 22	239: 249	249 259	93 99	325	1.7
22:	259:	269	9:5	1000:-	2.2:
22	269	279	9:7	18	0.7
7 7	279 ⁹	289	9. 3	14	0.3
22	289	299	9.9	23	0.7
22	299	309	9.9 9.9	7 57	0.4 1.0
22 22	309 319	319 329	9,9	175	0.9
22.	329	339	9.9	210	1.1
22	339	349	9.8	14	0.5
22	349	355	6.0	17	1.3

DDH	FROM (ft.)	TO (ft.)	RECOVERY (ft.)	Sn (ppm)	Ag (ppm)
22.	355	. 365	9.9	395	1.2
22	365	375	9.7	12	0.3
22	375	385	9.9	14	0.4
22	385	390	5.0	19	0.2
22	390	400	9.2	130	1.1
22	400	410	9.8	2010	1.8
22	410	420	9.8	27	0.4
22	420	430	9.9	540	0.7
22	430:	440:	9.9	18	0.4
	440	450	9.8	16	0.3
22 22	450	460	9.8	38	0.4
22	460	470	9.6	17	0.3
22	470	480	10.1	6	0.2
22	480	490	9.9	15	0.3
22	490	500 :	9.9	19	0.2
22	500	510	10.0	15	0.3
22	510	520	9.9	22	0.3
22 22	520	.530 542	9.8	12	0.2
22	530	555	11.1	57	0.4
23	542		12.2	14	0.2
23	4	10	5.5	70:	1.2
23	10	20	9.8	325	1.0
23	20	30:	9,9	3450	1.7
23	30	40	10.0	110	0.7
	40 50	50 60	10.0 10.0	63	0.5 0.4
23.	60	70	10.1.	25 20	0.3
23	70	80	10.0	28	0.3
23	80	98	9.9	36	2.5
23	90	100	9.8	32	0.2
23	100	110	9.9	145	0.7
23	110	120	9.9	45	0ے
23	120	130	9.9	100:	0.2
23	130	140	9.3	45 24	0.4
23 23	140 150	150 160	9.0 9.8 3.1	40	0.4 1.1
23.	160	165	3.1	65	0.5
23	165	175	9.2	475	50.0
23	175	182	5.6	2270	0.9
23	182	186	3.5	83	2.6
23	186	196	6.5	150	1.0
23	196	206	6.9	25	0.9
23	206	216	8.5	325	2.2
23	216	226	8.9	39	0.9
23	226	236	9.8	740	1.3
23	236	246	10.1	95	0.6
23	246	256	9.9	85	0.6
23	256	266	9.5	275	4.8
23	256	27 6	9.9	230	1.2
23	276	286	9.0	140	0.8
23	286	296	10.0	58:	0.9
23	296	306	10.1	350	12.0
23	306:	316:	9.9	37	0.5
23	316	326	9.8	24	0.7
23	326	336	9.6	500	6.4
23	336	346	10.2	16	0.4
23	346 356	356 366	9.9 10.0	24 1000	0.4
23 23	336 366	376	9.7	65	1.6 0.8

DDH	FROM (ft.)	TO (ft.)	RECOVERY (ft.)	Sn (ppm)	Ag (ppm)
23	376	386	9.7	670	1.4
23	386	396	9.2 9.4	17 30	0.4 0.4
23 23	396 406	406 418	11.8	21:	0.4
23	418	428	9.7	6350	6.8
23	428::	438	9.2	19 60	4.1
23	438	448	8.4	145	2.0
23	448	453	4.9	1050	2.0
23	453	463	9.8	54	0.9
23	463	468	4.9	17	0.7
23	468	478	10.2	12	0.3
23	478:	488	10.1	27	3.1
23	488	498	10.1	22	0.5
23	498:	508	9.7	S	ک0
23	508	513	4.6	14	کـ0
23	513	523	9.8.	340:	2.0
23	523	533	9.4	5	0.2
23	533	543	9:0*	165	0.4
	543	553	8.0	445	0.4
23 23	553	558	5.0	27	0.5
23	558	568	9.2	30	0.3
23	568	578	9.9	9	0.2
23	578	588	9.9	7	0.2
23	588	598	10.0	9	0.2
23	598	608	9.8	10	0.2
23	608:	618	9.8:	9:	0.2
23	618	628	9.8	5	0.2
23	628	638	9.9	12	0.2
23	638	648	9.6	8	0.2
23	648	653	9.3	22	0.3:
23	658	668	8.5	160	2.0
	668	678	10.0	26	0.8
23 23	678	688	9.7 3.7	205 9:	4.2 0.6
23 24	688 10	693. 15	4.6	1025	2.2
2 4 24	. 15	25:	9.3	230::.	4.5
	. 25	35	10.0	97	5.0
24	35	4 0 :-	5.0	24:	0.7
24	40	47	7.0	22	0.5
24	47	52	5.0°	1050:	1.2
24	52	62	9.7	1600	2.4
24	62:	72:	9.E	155.	0.8
	72	82	10.0	210	2.0
24	82 :	87:	4.9	205:	2.7°
24		92	4.8	240	1.4
24 24	87 92	102	9.7	940:	25: 22
24	102	107	4.9	550	59 %
24	107	112	5.0	19 0 ::	
24	112	122	9,9	83	1.7
24	122:	132	9,8	32	54.
24	132	· 142	9.9	68	0.9
24	142:		10.0	53:	2.6
24	152	162	9.9	185	4.0
24	162	172	9.9:	330:	1.3
24	172	182 192	9.9 9.0	125 425	1.5 0.5
24	182	202	8.0	59	0.7
24	192		6.4	35 5	0.8
Z4 24	20 2 212	212 222	9.0	16	0.8

DDH	FROM (ft.)	TO (ft.)	RECOVERY (ft.)	Sn (ppm)	Ag (ppm)
24	222	227	2.8	Adoministrativas raises and a service	
24 24	227	235	7.5	18 62	0.6 0.9
24	235 240	240 245	4.8 4.6	21 345	0.6 1.4
24 24	245 255	255 265	5.I	11	0.6
24	265	270	7.7 4.9	17 94	0.4 0.7
24 24	270 275	275 283	4.6 7.8	9 60	0.5
24	283	293	7.8	1900	0.6 1.3
24 24	293 303	303 313	9.2. 9.6	43 <i>5</i> 210	0.9
24 24	313 318	318	5.2	985	1.2 2.2
24	318 323	323 328	5.0 4.9	5400 2300	5.4 0.7
24 24	328 338	338 343	9.8 4.9	635	5.6
24	343	353	9.7	210 3500	2.2 22.0
24 24	353 358	358: 363	4.2 4.9	975 49	12.0
24	363	373	99	150	4.2 3.0
24 24	373 383	383 3 93	9.8 9.8	890 200	3.6 1.2
24 24	393 403	403	9.8	42	1.2
24	413	413 423	9:8 ک	2860 1630	15.0 3.4
24 24	423 433	433 438	6.0 4.9	835 1620	6.4
24	443	448	4.5	1570	11.0 5.6
24 24	448 458	458 468	72 77	650 395	6.2 1.1
24 24	468 478	478 485	9.7	1600	7.5
24	485	485 495	6.B 9.B	77 1550	1.0 2.1
24 24	495 505	505 513	10.0 7.6	33 1200	0.5
24	513	523	9:7	1200 3200	1.4 7.3
24 24	523 528	528 538	4.6 8.2	995 941	2.6
24 24	538	548	8.6	1100	3.6 4.2
24	548 553	553 558	4.4 4.8	180 2120	0.9 4.1
24 24	558 568	.568 578	10.0 10.0	110	0.4
24	578	588	9.9	30 185	1.8 0.6
24 24	588 598	598 603	10.0 4.9	49 115	0.3
24 24	603	609	5.9	670	0.3 0.9
24	60 9 619	619 630	9.9 11.0	4800 6100	15.0 19.0
24 24	6 30 635	635 645	5.0	2250	2.0
24	645	650	9.8 4.9	1170 1790	0.5 6.3
24 24	650 655	655 665	5.0 9.9	33 270	0.3 1.0
24 24	665	670	5.0	390	1.6
24	670 680	680 685	10.0 4.9	1580 2110	7.0 3.3
24	685	691	5.9	3740	3.2

DDH	FROM (ft.)	TO (ft.)	RECOVERY (ft.)	Sn (ppm)	Ag (ppm)
24	691	701	9.9	105	0.6
24 24	701	711 721	9.8	19	0.4
24	711 721	731	9.9 10.0	150 45:	0.4 0.4
24 24	731 741	741 751	10.0 10.0	115 17:	0.4 0.4
24 24	751	761	10.0	25	0.5
24	761 771	771. 779	10.0 8.0	125 165	0.3 1.6
24 24	779 789	789 795	9.7 5.8	695 7790	3.7 3.7
24	795	803	6.7	99 99	3.4
25 25	11 20	20 30:	3.9 8.5	38 27	0.6 0.7
25 25	30 40:	40 50	4.0 9.0	21 80:	0.8
25	50	60	8.2	44	1.3 3.0
25 25	60: 70	70: 80	7;4 1.5	4 1 . 76	29 6.5
25 25	80 90	90 100	4.2: 8.6	9 8 31.5	4.8 3.9
25.	100	110	7.8	2010	8.9
25 25	110 120:	120 130	9.9 6.2	70 75	3.9 1.7
25 25.	130 140	140 150	4.4 5.8	31	2.4
25	150	160	8.7	1700 51	5.9 2.6
25 25	160× 170	170 180	9,4 8.1	160: 35	3.0 1.5
25 25	180 190	190: 200	8.7	75	13
25:	200	210	10.1 9.1	760 195	5.7 3.4
25 25	210 220:	220 230	8.8 9.1	580 23 5	3.7 1.7
25 25:	230 240	240 250:	9.7 9.7	100	1.0 1.0
25	250	260	9.3	27 30	1.4
25 25	260: 270	270 275	9,9 5.0	34: 30	8.0 8.0
25 25	275: 287	28 7 297	9.8	2160	5.9
25:	297	307	9.7 9.8	1000 1000:	4.0 1.8
25 25	307 318	318 3 29	10.8 10.6	3250 5 90 ::	14.0 3.0
25 2 5	329 339	339 344	9.5 4.8	235	4.1
25 25	344	345	9.8	2550: 1750	7.6. 12.0
25. 25	354: 364	364: 374	9.9: 9.6	10 20 :: 130	3.7° 1.2
25:	374	384	9.8:	685	2.0.
25 25:	384 396	396 ** 408	11.9 11.8	490 2500	1_3 9.1
25 25 25	408 418	418 428	9.9 9.8	250 855:	18.0 1.0
25 25	428 437	437 447	8.6 10.0	360	1.5
25	447	457	10.0	10 50 % 26 50	7.7 35.0
25 25	457 465	465 470	7.8 4.9	310 69	0.9 0.8

DDH	FROM (ft.)	TO (ft.)	RECOVERY (ft.)	Sn (ppm)	Ag (ppm)
25	470	480	9.9	780	15.0
25	480	485	5.0	14	0.4
25	485	490	4.8	750	19.0
25 25	490 600	500 510	9.7	750 1 350	1.1
25	500 510	515	10.1 5.0	105	1.7 0.6
25	515	520	4.9	335	14.0
25	520	525	4.8	5600	10.0
25 25	525 626	530	4.7	2000	1.7
25 25	530 540	540 551	9.6 10. 9	2500 2100	13.0 4.6
25	<i>55</i> 1	561	9.9	540	2.4
25	561	570	9.0	1100	3.7
25 25	570	575	5.0	1560	6.6
25 25	57 <i>5</i> 580	580 590	5;0 10.0	975 315	1.9 0.4
25	590	601	11.0	4150	11.0
25	601	610	8.6	3700	7.6
25	610	615	4.6	880	7.6
25 25	61.5 620	620 630	4.9 10.0	2250 3600	4.6 0.5
25	630	635	4.9	1560	0.4
25	635	640	5.0	3350	0.9
25	640	650	9.9	180	0.3
25 25	650: 660	660 670	9;4 9.0	195 395	0.2 10.0
25	670	675	4.6	2250	2.0
25	675	680	4.9	6700	25.0
25	680	685	4,9	2150	13.0
25 25	685 690	690 695	5.3 5.0	2900 920:	18.0 0.7
25 25	695	705	9.1	105	0.2
25	705	715	10.2	39	0.2
25	715	725	9.8	60	0.2
25 25	725 735	735 745	9.9 10.0	17 32	0.2 0.2
25 25	745	755	10.0	59 ⁹	0.2
25	755	765	9.9	455	0.3
25	765	775	9.7	9	0.3
25 25	775 785	785 795	9.9 10.0	27 390	0.3 0.6
25	795	800	53	13	ک.0
	16	30		130	0.5
26°	30	40		5	0.7
26	40	.50 		5	0.8
26 26	50 60	60 70		6 7	0.9 0.8
26	70	80			
30	96	106	9.7	57	ک.0
30	106	117	8.5 8.1	40	0.9
30 30	117 125	. 125 134	8.2	80: 93	0.3 0.6
31	7	18	94	31.	1.0
31	18	28	9.7	43	1.7
31	28:	38	9.8	41	0.4
31 31	38 48	48 58	9.8 8.9	18 24	0.4 0.4
31	58	68	9.9	145	8.0
31	68	78	95	92	20

DDH	FROM (ft.)	TO (ft.)	RECOVERY (ft.)	Sn (ppm)	Ag (ppm)
31	78	. 88	9.2	240	4.0
31 31	88	98	9.6	27	8.0
31	98 108	108 118	9.7 9.8	155 3 35	1.7 3.0
31 31	118	128	9.8	360	4.6
31	128 138	138 148	9.7 8.8	235 1 <i>9</i> 30	11.0 20.0
31 31	148	158	8.2	660	28.0
31	158 168	168 178	6.7 4.3	120 350	2.2 11.0
31	178	188	2.7	160	15.0
31 31	188 198	198 205	3.8 4.1	165 66	1.6 1.6
31	205	218	10.1	70	1.6
31 31	218 228	228 238:	9.0 9.5	54 74	1.1
31	238	248	9.5	72	0.6 0.7
31 31	248:: 255	255 265	6.4: 7.1	58 105	0.7
31	265	273	4.0	50:	3.9 1.0
31 31	273 283	283 293	6.7 4.5	65 115	1.2
31	293	303	8.4	54	2.6 0.7
31. 31	303 313	313 323	9.8: 7.0	45 40	8.0
31	323	333	9.6	36	0.4 0.4
31 31	333 343	343 353	10.1 9.9	340 26	8.0
31	353	363	9 . 5	25 55	0.6 0.5
31. 31	363 373	373 383	10.0 10.0	45	ک.0
31	383	393	9.B	110 130	0.4 0.3
31 31	393 403	403 413	9.7 9.8	63	1.8
31	413	418	5.0	750 97	1.2 0.5
3 2 :::32	3. 13	13:	93	2400	13
3 2	23	23 33	9.9 9.7	795 2110	2.6 2.4
32 32	33 43	43 53	9.7	3300	13.0
32	53	63	9 <u>.</u> 9: 9.8	365 2200	7.3 31.0
3 2 32	63 68	68	4.9	850	93
3 Z	78	78 88	10.0 9.9	9300 2640	38.0 18.0
32 32.	88 98	98	10.0	4190	25.0
32	98 108	108 118	9. 9 % 10.0	2870 1110	40:0 23.0
32	118	128	9.4:	1250	130
32 32	128 140::	140 150:	5.6 9.2:	1165 340	5.4 1.8
32	150	160	9.3	410	29
32° 32	160: '	″ 170% 180	9 5 . 9.8	210: 5100	5.4. 27.0
32: 32	180	190»	10.0	120	1.0:
3Z 3Z	190 200:::	200 207	8.8 4.2	245 37 5	25 24
32 32	207	217	5.6	1800	8.0
32	217: 225	27.5 232	7.2 6.3	12 2300	0.4 1.7

DDH	FROM (ft.)	TO (ft.)	RECOVERY (ft.) Sn (ppm)	Ag (ppm)
32	232	240	7.6	14	0.8
32	240	250 260	9.9 9.9	38 305	0.8 0.9
3 2 32	250 260	270 270	9.8	1880	1.0
32	270	280 200	9.9 10.0	125 91	1.0 0.4
32 32	280 290	290 300	10.0	920	0.5
32	300	305	5.0 9.8	360 1660	0.6 5.8
32 32	30 <i>5</i> 31 <i>5</i>	315 325	9.8	3200	5.5
32	325	335	9.8 9.3	165 215	1.1 1.0
32 32	335 345	345 355	95 95	12	8.0
32	355	360	4.5 9.6	16 4500	1.1 2.6
32 32	360 370	370 380	9.9	91	1.4
32	380	390	9:1	215	4.4 2.4
32 32	390 400	400 410	8.7 9.3	360 140	5.0
32 32	410	420	9.5	6000	7.8 22.0
32	420 425	425 435	4.6 9.7	3500 2200	3.0
32 32	435	445	9.9	900	5.0
32	445 455	455 465	9.7 9. 5	130 3500	1.4 50.0
32 32	433 465	475	9.4	460	2.7
32	475	480 490	4.7 10.0	3800 1920	8.6 5.0
32 32	480 490	500	10.0	3600	9.0
32	500	510	9.8 9.4	2680 3010	4.6 3.6
32 32	510 520	520 530	9.9	2750	6.6
32	530	540	10:1 10:0	3500 425	2:3 0.7
32 32	540 550	550 560	10.0	42	0.4
32	560	570	10.1	560 12	0.6 0.5
32 32	570 580	580 590	10.0 10.0	5	0.3
32	590	600	10:0	28	0.4 0.7
32	600 610	610 620	10.0 10.0	9 999 21	0.5
32 32	620	630	10.0	28	0.7
32 32	630 640	640 650	10:0 10.0	17 39	1.0 0.5 0.3
32 32	650	660	10.0	39 6	0.3
32	660 670	670 680	10.0 10.0	6 5	0.3 0.2
32 32	680	69 0	10.0	750	2.0
32	690 700	7 00 710	9.1 9.9	15 880	02 1.2
32 32	700 710	720	93	5	1.2 0.2
32	720	728	6.0 5.5	1650 20	1.3 0.5 1.7
33 33	3 10	10 20	9.7	2200	1.7
33	20 30	30	9:1 9:5	45 145	13 12 15
33 33	30 40	40 50	9.5	145 93	15
33	50 60:	60	9.2 9.8	175 220	2.9 3.6
33	60	70	7.0		600 000 01 0 PP 600 000 000 000 000 000 000 000 00

133	DDH	FROM (ft.)	TO (ft.)	RECOVERY (ft.)	Sn (ppm)	Ag (ppm)
33 90 100 10.0 32 0.7		70	80	10.0	100	2.4
33		Control of the Contro	111.00000 00450 To November		rannon como con esta esta esta esta esta esta esta esta	
33 110 120 7.9 80 3.1 33 120 130 5.6 225 12.0 33 130 140 3.3 580 19.0 33 130 160 170 7.6 2800 13.0 33 150 170 7.6 2800 10.0 3.6 33 170 180 8.5 1000 3.6 3.6 33 180 190 8.6 1800 5.2 3.6 33 120 20 9.8 1.55 4.7 3.6 5.2 3.3 100 5.2 3.3 1.00 5.2 3.3 3.0 5.2 3.3 3.0 5.2 3.3 3.0 5.2 3.3 3.0 5.2 3.3 3.0 3.0 5.2 3.3 3.0 3.0 3.0 9.9 2.0 3.5 3.3 3.9 3.3 3.9 3.3 3.0 3.0	1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.	 State of the second second comments of the second se			MANAGARAN SA	CONTRACTOR OF THE CONTRACTOR O
33 130 144 3.3 580 190 33 140 150 4.8 922m 13.0 33 150 160 170 7.6 2000 10.0 33 170 180 8.5 1000 3.6 33 180 190 200 9.8 1950 4.7 33 180 200 210 8.9 1950 4.7 33 220 220 9.4 705 5.2 33 220 220 9.7 855 3.9 33 220 220 9.7 855 3.9 33 220 220 9.7 855 3.9 33 250 250 9.9 2 0.5 33 250 250 9.9 2 0.5 33 250 250 9.9 2 0.5 33 250 250 9.9 2 0.5 33 250 250 9.5 105 1.4 33 270 280 9.5 105 1.2 33 290 300 9.5 105 1.2 33 320 300 9.7 855 3.9 33 250 5.5 100 9.7 855 3.9 33 250 5.5 100 9.7 855 3.9 33 250 5.5 100 9.7 855 3.9 33 250 770 9.7 855 1.0 33 250 770 1.0 33 250 770 1.0 33 32 250 250 9.5 105 1.2 33 32 250 300 9.5 105 1.2 33 32 300 310 9.2 105 1.2 33 32 300 310 9.2 105 1.3 33 300 340 9.7 205 1.8 33 300 300 300 9.7 205 1.8 33 300 300 300 9.7 200 9.7 33 300 300 300 9.7 200 9.7 300 9.7 200 9.7 200 9.7 300 9.7 200 9.7 200 9.7 300 9.7 200	33	110	120	7.9	80	3.1
133	2.1 (2004)202		AND THE PROPERTY OF THE PARTY O	The figure and the figure of t	A ANDROS SANTA TO TO TO THE SANTAN THE SA	Property of the second section of the section of th
33 150 160 7.2 1060 5.7 33 160 170 7.6 2800 10.0 33 170 180 8.5 1000 3.6 33 180 190 200 9.8 1950 5.2 33 190 200 9.8 1950 4.7 33 200 220 9.7 855 5.2 33 220 220 9.7 855 3.9 33 220 220 9.7 855 3.9 33 220 220 9.7 855 3.9 33 220 220 8.9 2200 5.0 33 220 20 9.5 200 9.5 33 220 20 9.5 200 4.5 33 200 30 9.5 105 12 33 30 30 30 9.7 205 3.8 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>						
33 170 180 8.5 1000 36 33 150 190 8.6 1800 52 33 190 200 9.8 1950 4.7 33 200 210 8.9 840 5.8 33 210 220 9.7 855 3.9 33 220 220 9.7 855 3.9 33 240 28.8 675 13.0 33 240 250 8.9 200 0.5 33 260 270 9.7 635 1.4 33 260 270 9.7 635 1.4 33 270 280 9.5 2800 4.9 33 280 290 9.5 2800 4.9 33 300 110 9.2 105 1.2 33 300 10 9.7 205 3.8 33 310<		************				5.7
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33. 637 647 10.0 18. 0.4	33	617	627	10.0*	12	0.3:
					13 18	

DDH	FROM (ft.)	TO (ft.)	RECOVERY (ft.)	Sn (ppm)	Ag (ppm)
34	470	480	9.8	74	0.5
34	480	490	9.9	24	0.3
34	490	500	9.9	12	0.7
34	500	510	10.0	10*	0.6
34	510	520	9.8	5	0.5
34	520	530	5.6	10	1.4
34	530	540	2.8	10	0.9
34	540	550	6.4	6.	1.8
34	550	560	10.1	35	3.0
34	560	570	9.8	28	2.8
34	570	580	10.0	10	0.3
34	580	593	12.9	6	0.2
35	1	10	6.8	110	1.5
35	10	20	9.5	1000	33
35	20	30	10.0	725	1.1
35	30	4 0	9.8	400	3.2
35	40	50	9.3	1200	2.9
35	50	60	9.8	1500	2.7
35	60	70	10.0	95	0.6
35	70	80	9.7	565	2.2
35	80	90	9.8	665	5.0
35	90:	95	4.9	1850	10.0
	95	100	5.0	1550	3.8
35 35	75 100 110	100 110 120	9.8 9.9	785 2400	2.3 12.0
35 3 5	120	125	5.0 9.7	910 505	17.0 3.7
35 35	125 135	135 140	4.6	315	4.2 7.4
35 35	140 145	145 155	4.8 10.0	452 860 875	7.4 3.9 5.0
35 35	155 165	165 175	10.0 9.9	455	2.8
35	175	185	9.8	500	2.7
35	185	195	9.7	815	5.3
35	195	205	9.9	1760	5.3
35	205	215	9.9	9 55	5.1
35	215	225	9.8	340	3.3
35	225	235	9.7	270	2.2
35 35 35	235 245	245 255	9.8 10.3	400 685	3.7 5.1
35	255	265	10.0	240	2.5
35	265	270:	4.8	48	1.4
35	270	280	9.5	260	2.8
35	280	285	4.6	140	2.6
35	285	295	9.2	440	2.1
35	295	305	9.8	570	4.6
35	305	315	9.7	185	1.9
35	315	325	9.6	135	1.1
35	325	335	10.0	700	2.2
35	335	345	9.7	330	1.5
35	345	355	9.7	175	0.9
35	355	365	7.5		1.1
35 35	365 375	375 385	6.4 9.0	275 23 20	کـ0 0.3
36	20	30	10.0	215	3.4
36	30	35	5.0	32:::	2.0
36	35	45	10.0	1530	7.8
36	45		10.0	750	3.0
36	55	65	9.8	340	3.1

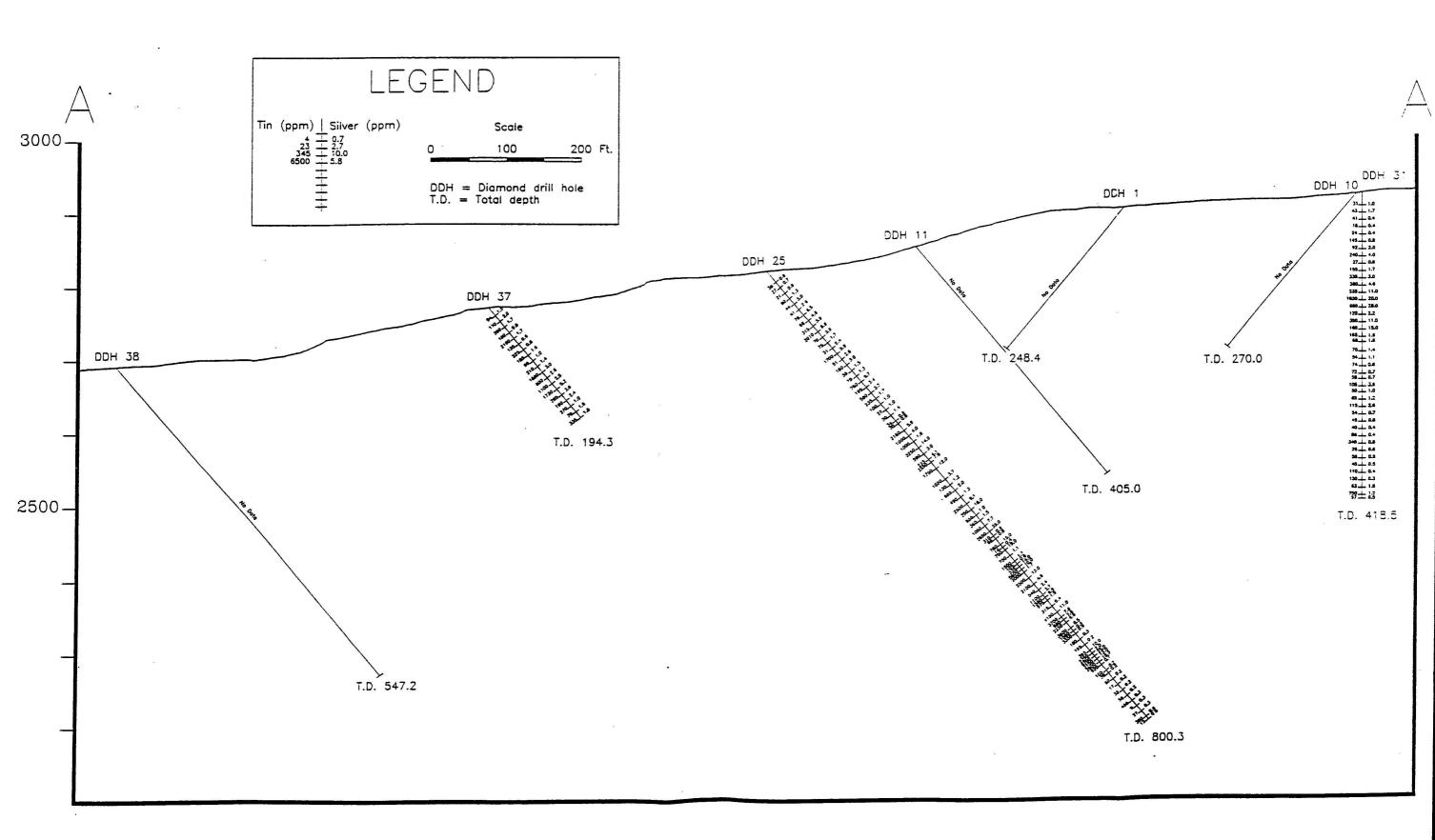
DDH FROM(ft.)	TO (ft.)	RECOVERY (ft.)	Sn (ppm)	Ag(ppm)
33 657	667	9.9	500 10	0.5 0.3
33 667 33 677	677 687	10.0 10.0 5.0	3 9999	0.2 5.5
33 687 33 692	692 702 712	9.9 9.6	365 275	0.8 0.6
33 702 33 712	717 727	4.8 8.3	110 5200	0.2 3.0
33 717 23 727 33 737	721 737 747	4.5 5.8	340: 61	0.4 0.5
33 737 34 5 34 15	15 15 25 25	10.1 9.6	610 545	2.7 1.4
34 25 34 35	35 45	92 9.7	335 125	1.0 0.2
34 45 34 55	55 65	9.8 9.9	2500: 500	0,4 10.0 19.0
34 65 34 75	75 85	9.7 9.7	3500° 2200 260°	9.1 5.8
34 85 34 90	90 100	4.9 8.3 5.6:	600 900	21 6.2
34 100 34 110	110 120 130	3.6 8.4 8.5	2900 265	3.4 6.3
34 120 34 130	140 150	3.8 8.9	100 1440:-	20 25
34 1408 34 150 34 160	160 170	8.9 7.7	150 130:	0.4 1.5
34 160 34 170 34 180	180 190	8.7 9:2	2800 190	1.2 0.8
34 190 34 200	200 210:	9.3 9.3	3200 46	0.5 0.6
34 210 34 220	220 230	9.7 9. 2	24 36	0.9 E.O: 1.0
34 230 34 235	235 245	4.8 9.5	17 28 : 75	0.4: 1.6
34 245 34 255	255 265	9.5 6.5 2.9	35 5	0.2 0.4
34 265 34 270	270 280 290	85 4.4	40 5	0.6 0.3
34 280 34 290	300 310	8.7 9.7	8	0.5 0.4
34 300 34 310 34 320	320: 330	9.5. 9.7	5 5 26	0.4 0.6
34 320 34 330 34 340	34 0 350	9.7	15 18	کہ کہ
34 350 34 360	360° 370	9.8 9.3 8.5	16 8	0.3 0.4 0.4
34 370 34 380	380 390	9.7 9.6	13 10	0.5 0.7
34 390 34 400	400 410	8.7 7.9	8% 50 350%	0.2 0.6 1.0
34 410 34 420	420 430	95 95 94	30 15	0.7 0.5
34 430 34 440	440 445 455	4.2 7.2	48 1120	0.4 0.8
34 445 34 455 34 465	465 470	7.7 4.8	25 18	0.5 0.7

DDH	FROM (ft.)	TO (ft.)	RECOVERY (ft.)	Sn (ppm)	Ag (ppm)
36	65	.75	9.3	1610	1.8
36 36	75 85	85 90	9.8	85 310	1.2 3.6
36	90	50 100	4.8 9.7	310 1810	3.0 11.0
36	100	105	48	1600	3.7
36 36	105 115	115 125	9.6 9.9	910 1500	4.4 11.0
36	125	135	9.7	1940	13.0
36 36	135 145	145 155	9.2 7.6	39 5 460	45
36	155	165	7.8 8.0	140	3.6 2.0
36	165	170	4.8	125	2.6
36 36	170 180	180 190	10.0 10.0	1510 - 5590	14.0 2.5
36	190	200	9.8	1910	11.0
36	200	210	8.1	46	1.3
36 36	210 220	220 225	8:2 4.5	425 810	1.4 1.4
36	225	235	8.1	2370	11.0
36 36	235 245	245 255	10.0 7.0	2090 680	15.0 3.3
36	255	265	9.6	1160	55 55
36	265	275.	9.7	3590	6.5
36 36	275 285	285 295	9.7 10.0	2970 2010	13.0 12.0
36	295	304	8.9	2410	14.0
36	304 23.4	314	9:7	4160	15.0
36 36	314 323	323 331	9.0 8.0	2620 110	18.0 1.4
36	331	337	6.0	210	0.6
36 36	337 344	344 354	7.0 10.0	285 840	3.0 1.2
36	354	364	10.0	3780	20.0
36	365	369	5.0	7150	26.0
36 36	369 374	374 384	4.9 9.8	3740 2440	2.2 19.0
36	384	394	9.9	710	15
36 36	394 404	404 414	9.8 9.8	215 100	2.5 1.0
36	414	424	9.9	325	24
36	424	434	9.7	220	8.0
36 36	434 43 9	439 449	4.9 9.9	595 31	3.2 2.2
36	449	459	8.9	56	0.6
36 26	459	469	10.0	175	0.5
36 36	469 479	479 489	10.0 10.0	475 270	1.8 1.2
36	489	499	10.0	67	0.8
36 36	499 509	509 519	9;9 9.4	200: 20	0.8 کـ0
36	519	525	5.4 6.0	2590:	17.0
36	525	535	9.6	680	4.3
36 36	535 542	54 2 552	7.0 9.7	2110 2510	9.4 11.0
36	552	562	8.8	9999	9.5
36	562	572 582	9.3	960 105	1.0
36 36	572 582	582 592	8.3 9.2	105 2250	0.6 1.6
36	592	602	8.2	1700	3.6

DDH	FROM (ft.)	TO (ft.)	RECOVERY (ft.)	Sn (ppm)	Ag (ppm)
36	602	612	8.2	2510	8.3
36	612	620	5.6	3290	4.0
36 36	620 62 5	625 635	3.9 9.2	5650 2680	35.0
36	635	645	<u>74.</u>	260 960	20.0 4.2
36	645	655	9.0	270	1.1
36	655	665	8.5	790	3.8
36 36	665 675	675 685	9.6 9.2	1300 31	1.4 0.5
36	685	695	9.7	320	1.8
36	695	705	9.5	970	1.9
36 36	705 715	715 725	9.2 9.6	33 <i>5</i> 89	1.4
36	725	735	9.3:	260	0.4 6:2:
36	735	745	9.8	1300	8.0
36	745	755	9,6	100	0.5
36 37	755 4	762 14	6.8 8.2	86 94:	1.0 1.5
37	14	24	7.8	110	2.0
37	24	34	9.6	290	1.7
37	34 44	44 54	9.6	180	0.8
37 37	5 4	54 64	9.7 9.6	2190 135	1.7 0.6
37	64	74	10.0	225	0.6
37	74	84	9.3	185	1.6
37 37	84 94	94: 104	10.0 9.8	89: 210	1.0 1.4
37	104	114	9.8	1680	3.0
37	114	124	9.5	600	2.6
37 37	124 134	134 144	9.6 9.4	1100 1730	25 52
37 37	144	154	7.4 7.5	295	3.6
37	154	164	2.8	190	24
37	164	174	61	270	1.0
37 37	174 184	184 194	4.6 4.8	70 335	1.6 1.8
39	. 6	12	4.7	320	2.6
39	12	21	8.0	96	1.5
39 39	21 31	31 41	7.2	260	1.8
39	41	S1	93 78	120 250	0.6 1.8
39	51	61	72	220	2.0:
39	61	71 81	4.6	1630	16.0
39 39	7 1 81	81 91	9.8 9.7	690: 1300	8.0 5.0
39	91°	101	9.7 93	150	1.2
39	101	111	8.5	830	1.1
39	131	140	9.1	75	1.6
39 39	140 150	150 160	10.1 10.2	105 180:	1.4 1.7
39	160	. 170	10.0	140	23
39	170	180	9.6	605:	4.2
39 39	180 190	190 200	9.8 9.9	47 87	2.0 1.2:
39	190 200	209	9.1	74	1.2 1.2
39*	209	220	11.0	1000	12.0
39	220	230	10.0	7340	5.4
39 39	230 240	240 250	10.0 10.1	380 260	4.3 7.6
	2.0				

DDH	FROM (ft.)	TO (ft.)	RECOVERY (ft.)	Sn (ppm)	Ag (ppm)
39	250	- 260	10.1	1800	2.6
39	260	270	10.0	855	6.7
39	270	280	9.6	375	2.6
39	280	290	9.3	1530	4.8
39 39	290 300	300 310	9.9 8.9	415 1820	6.5 9.6
39	310	320	9.9	550	6.2
39	320	330	9.9	3650	19.0
39	330 340	340 350	10.0 9.9	500 1890	7.4 5.8
39 3 9	350	359	93 95	890	3.5 1.9
39	359	369	9.9	115	1.4
39	369	379	10.0	850	8.6
39 39	379 389	389 401	10.0 12.1	520 1600	4.8 16.0
39	401	408	6.9	3180	3.1
39	408	415	6.9	145	1.4
39	415	422	6.9	3030	31.0
39 39	422 432	432 442	10.0 10.0	1810 485	9.8 5.3
3 9	442.	452	10.0	270	22
39	452	462	9.9	1.530	5.0
39	462	467	4.8	72	0.6
39 39	467 477	477 487	9.8 10.0	40 53	1.8 0.2
39	487	497	9.9		0.7
39	497	507	10:1	87	0.2
39	507	517	9.8	63	0.2
39 39	517 537	527 537	9:7 9:9	40 49	0.2 0.6
39 39	527 537	337 547	2.5 8.5	120	0.0
39	547	554	7.2	82	0.2
39	554	565	8.4	330	1.7
39 39	580 590	590 600:	4.8 8.2	33 1630	0.3 1.3
3 9	600	610	9.0	1130	5.6
39	. 610	620	8.0	42.	0.4
39	620	6 3 0	7.0	57	0.4
39 39	630 635	635 645	1.7 7.1	295 8	18.0 0.2
41	75	85	6.4	250	1.4
41	85	95	7.4	29	2.0
41	95	105	7.0	44	2.0
41 41	105 125	125 135	9.7 9.6	350 280	1.9 1.1
41	135	145	9.9	355	0.7
41	145	155	10.2	385	0.6
41	155	165	10.1	200	0.6
41 41	165 175	175 185	10.0 10.2	165 125	0.9 0.8
41	185	195	10.1	320°	0.7
41	195 205	205 715	9.8 10.7	245 105	1.2

Appendix C. N15E cross section with assay data



Appendix D. N15E cross section with assay data

